



# An amperometric NO<sub>2</sub> sensor based on nano-structured La<sub>0.75</sub>Sr<sub>0.25</sub>Cr<sub>0.5</sub>Mn<sub>0.5</sub>O<sub>3-δ</sub> prepared by impregnating method

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La<sub>0.75</sub>Sr<sub>0.25</sub>Cr<sub>0.5</sub>Mn<sub>0.5</sub>O<sub>3-δ</sub>

## ABSTRACT

An amperometric NO<sub>2</sub> sensor using nano-structured perovskite-type oxide La<sub>0.75</sub>Sr<sub>0.25</sub>Cr<sub>0.5</sub>Mn<sub>0.5</sub>O<sub>3-δ</sub> (LSCM) as sensing electrode with Ce<sub>0.9</sub>Gd<sub>0.1</sub>O<sub>1.95</sub> (CGO) electrolyte was fabricated. The LSCM particles were prepared in the porous CGO layer by impregnating method. The composition and microstructure of the sample were characterized by XRD and SEM, respectively. The properties of the sensor for monitoring NO<sub>2</sub> were studied. The results showed that the LSCM particles in the range of 50–150 nm were homogeneously dispersed in the porous CGO layer. The response current was almost linear to NO<sub>2</sub> concentration in the range between 20 and 300 ppm. With the temperatures increasing, the sensitivity increased and reached 111.36 nA ppm<sup>-1</sup> at 500 °C. The sensor showed good response, recovery, reproducibility and stability. Although the response current was slightly affected by changing O<sub>2</sub> concentrations in the range of 0–10 vol%, the influence was negligibly small.

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## 1. Introduction

Nitrogen dioxide (NO<sub>2</sub>), which is emitted from the exhaust gas of automotive engines, boilers, and any other combustion facilities into the atmosphere, is one of the main causes of air pollution and highly harmful for human beings [1,2]. Therefore, it is necessary to develop high performance NO<sub>2</sub> sensors for monitoring the exhaust gas from automobiles and factories. For this purpose, a special attention has been paid to the solid electrolyte type NO<sub>2</sub> sensors which are available on detection of NO<sub>2</sub> using either the potentiometric [3–8], the impedancemetric [9–14] or the amperometric mode [15–20] with fast response, high sensibility and good stability.

In order to improve the properties of the NO<sub>2</sub> sensors further, nano-structured sensing electrodes have attracted many interests of researchers [21–24]. It has been proposed that the utilization of nano-structured sensing electrodes means the increasing length of the triple phase boundary (gas/sensing electrode/electrolyte) and high catalytic activities to NO<sub>2</sub>, which leads to improve the sensitivity, stability and anti-interference. Plashnitsa et al. [21,22] reported the novel mixed-potential-type planar sensors using nano-structured NiO-Ses, which obtain a large enhancement in both sensitivity and selectivity to NO<sub>2</sub>. Xiong and Kale [23] used

nano-structured CuO + CuCr<sub>2</sub>O<sub>4</sub> mixed-oxides as sensing electrode. The EMF (electromotive force) response of the sensor was highly reproducible to change in concentration of NO<sub>2</sub> and the sensor also showed negligible cross-sensitivity to O<sub>2</sub>, CO and CH<sub>4</sub>. Martin et al. [24] investigated an impedancemetric method for NO<sub>2</sub> sensing using nano-sized YSZ (yttria-stabilized zirconia)/Cr<sub>2</sub>O<sub>3</sub> composite electrodes and found that the sensing performance of the sensor was affected by the surface topography of sensing electrodes. In the meanwhile, the triple phase boundary also can be increased by designing and controlling the surface roughness of the electrolyte. Liang et al. [25] fabricated a mixed-potential-type NO<sub>2</sub> sensor using YSZ plate corroded by hydrofluoric acid as electrolyte to increase the triple phase boundary and the selectivity and rapid response–recovery characteristics of the NO<sub>2</sub> sensor were improved.

As mentioned above, the nano-structured sensing electrodes can improve performance of potentiometric and impedancemetric sensors. It is reasonable that the nano-structured sensing electrodes should also be used to enhance characteristics of the amperometric NO<sub>2</sub> sensor. In this paper, an amperometric NO<sub>2</sub> sensor based on measuring currents upon application of a cathodic potential to nano-structured LSCM sensing electrode and Pt counter electrode on a CGO electrolyte for detecting NO<sub>2</sub> was proposed. The nano-structured LSCM particles were prepared in the porous CGO layer by impregnating method which is a well-known method in the development of heterogeneous catalysts for solid oxide fuel cells [26–29]. The detailed sensing characteristics of the sensor are reported and discussed here.

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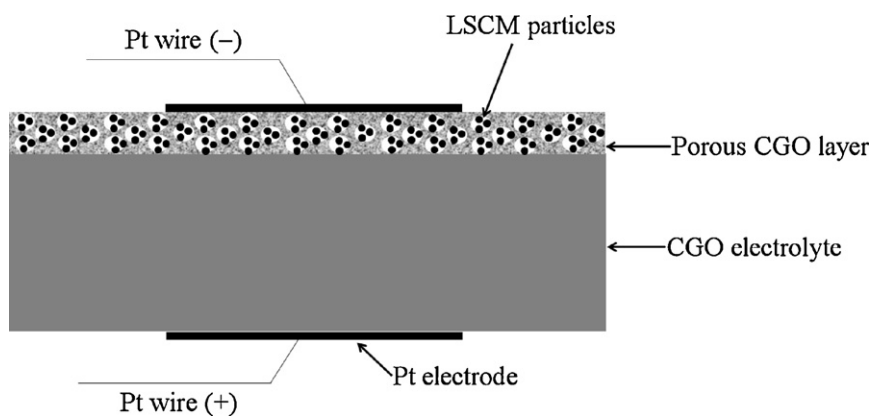


Fig. 1. Schematic view of the sensor.

## 2. Experimental

### 2.1. Preparation of CGO electrolyte and its porous CGO layer

Analytically pure  $\text{CeO}_2$  and  $\text{Gd}_2\text{O}_3$  were mixed with ethanol and ball-milled for 24 h and then calcined at  $950^\circ\text{C}$  for 5 h in air. The milling-calcining cycle was repeated for three times. The calcined powders were pressed into pellets (about 10 mm in diameter, 2 mm thickness) and then sintered at  $1600^\circ\text{C}$  for 5 h to form dense CGO electrolyte.

The porous CGO layer on the surface of above-mentioned dense CGO pellets was prepared by screen printing technique and then sintered at  $1450^\circ\text{C}$  for 5 h. The ink used in screen-printing was prepared by dispersing CGO powder with 30 wt.% pore-forming agent (graphite powder) into an organic vehicle (terpineol, 94 wt.% and ethylcellulose, 6 wt.%).

### 2.2. Sensor fabrication and characterization

The LSCM nanoparticles used as sensing materials were introduced into the Porous CGO layer by impregnating technique. Firstly,  $1\text{ mol}\cdot\text{L}^{-1}$  LSCM precursor solution for impregnation was prepared by adding  $\text{La}(\text{NO}_3)_3\cdot 6\text{H}_2\text{O}$ ,  $\text{Sr}(\text{NO}_3)_2$ ,  $\text{Cr}(\text{NO}_3)_3\cdot 9\text{H}_2\text{O}$  and  $\text{Mn}(\text{NO}_3)_2\cdot 4\text{H}_2\text{O}$  to deionized water according to molar ratio 0.75:0.25:0.5:0.5. Secondly, the LSCM precursor solution was pipetted into porous layer of the samples with  $4\ \mu\text{L}$  of solution at a time, followed by drying in an oven at  $100^\circ\text{C}$ . The impregnating-drying cycle was repeated for five times. After impregnation, the sample was calcined at  $800^\circ\text{C}$  for 3 h in air to decompose nitrate salts and produce the perovskite LSCM phase. The LSCM loading was about 4.6 mg. Pt paste was painted on the two sides of sample. Pt wires were used to make contact with the sensor, as shown in Fig. 1. The composition and microstructure of the sample were characterized by X-ray diffraction with Cu-K $\alpha$  radiation (XRD, D/MAX2500PC) and field emission scanning electron microscopy (SEM, S-4800), respectively.

### 2.3. Evaluation of sensing properties

$\text{NO}_2$  sensing properties were tested in a gas flow apparatus with heating tube furnace in the temperature range  $400\text{--}550^\circ\text{C}$ . The gas environment consisted of a changing concentration of  $\text{NO}_2$  (0–300 ppm) with base gases ( $\text{O}_2 + \text{N}_2$  balance) at a total flow rate of  $100\text{ cm}^3/\text{min}$ . The current-potential characteristics of sensors were measured by potentiodynamic method at a constant scan-rate of  $1\text{ mV/s}$  in the potential rang from 0 to  $-300\text{ mV}$  by using a two-electrode configuration. The amperometric responses of the sensor were measured by potentiostatic method at  $-300\text{ mV}$ . The complex-impedance measurements of the sensor were performed in the frequency range of 0.1–1 MHz with a  $50\text{ mV}$  amplitude ac signal. The fore-mentioned all electrochemical measurements were performed by the electrochemical workstation (Zahner IM6e).

## 3. Results and discussion

### 3.1. Characterization of the sensor materials

Fig. 2 shows the XRD patterns of the porous layer without and with LSCM-impregnation. The porous framework displayed a single CGO phase before LSCM-impregnation (Fig. 2A). There was no peak of carbon as pore-former in XRD pattern, which manifested that carbon had been removed during sintering process. After

impregnation and fired at  $800^\circ\text{C}$  for 3 h, perovskite LSCM phase can form and no other phase appears (Fig. 2B).

SEM micrographs of surfaces and fractured cross-sections of the sensor without and with LSCM-impregnation are shown in Fig. 3. The original CGO porous layer showed a uniform, porous and three-dimensional network structure with sub-micron pores (Fig. 3A), which was a result due to the oxidation of pore-forming agent (graphite powder). As seen in Fig. 3B, the porous layer was combined with dense CGO solid electrolyte substrate tightly after sintering. The thickness of porous layer after 3 times printing was about  $25\text{--}30\ \mu\text{m}$ . After LSCM impregnation, the representative SEM images of surface and cross-section of the sensing electrode are shown in Fig. 3C and D. It was seen that the LSCM particles were uniformly dispersed in the CGO backbone and deposited not only on the surface of the porous layer but also throughout the CGO backbone. Very fine LSCM particles were formed around CGO backbone and their size was in the range of  $50\text{--}150\text{ nm}$  (Fig. 3E). Because sensing material LSCM made contact with CGO electrolyte in three-dimensional structure, the triple phase boundary length (the  $\text{NO}_2$  gas/LSCM electrode/CGO electrolyte) was greatly enhanced, which means increasing number of gas reaction sites and brings about the improvement of the response for the sensor. It is speculated that the sample gas can diffuse easily into the SE layer due to its high porosity and  $\text{NO}_2$  gas can be easily reduced because of the presence of monodispersed nanocrystalline LSCM particles.

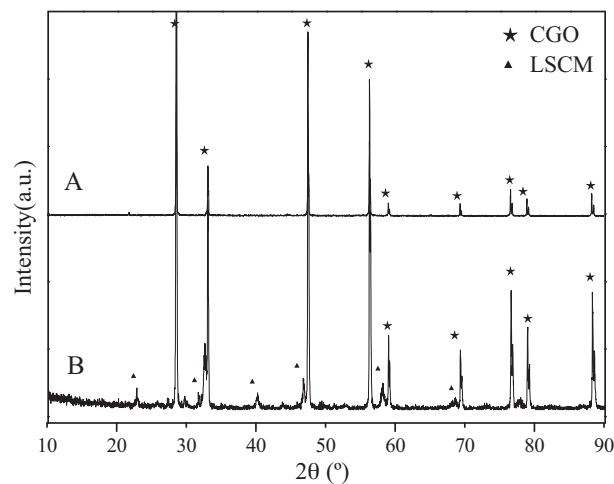
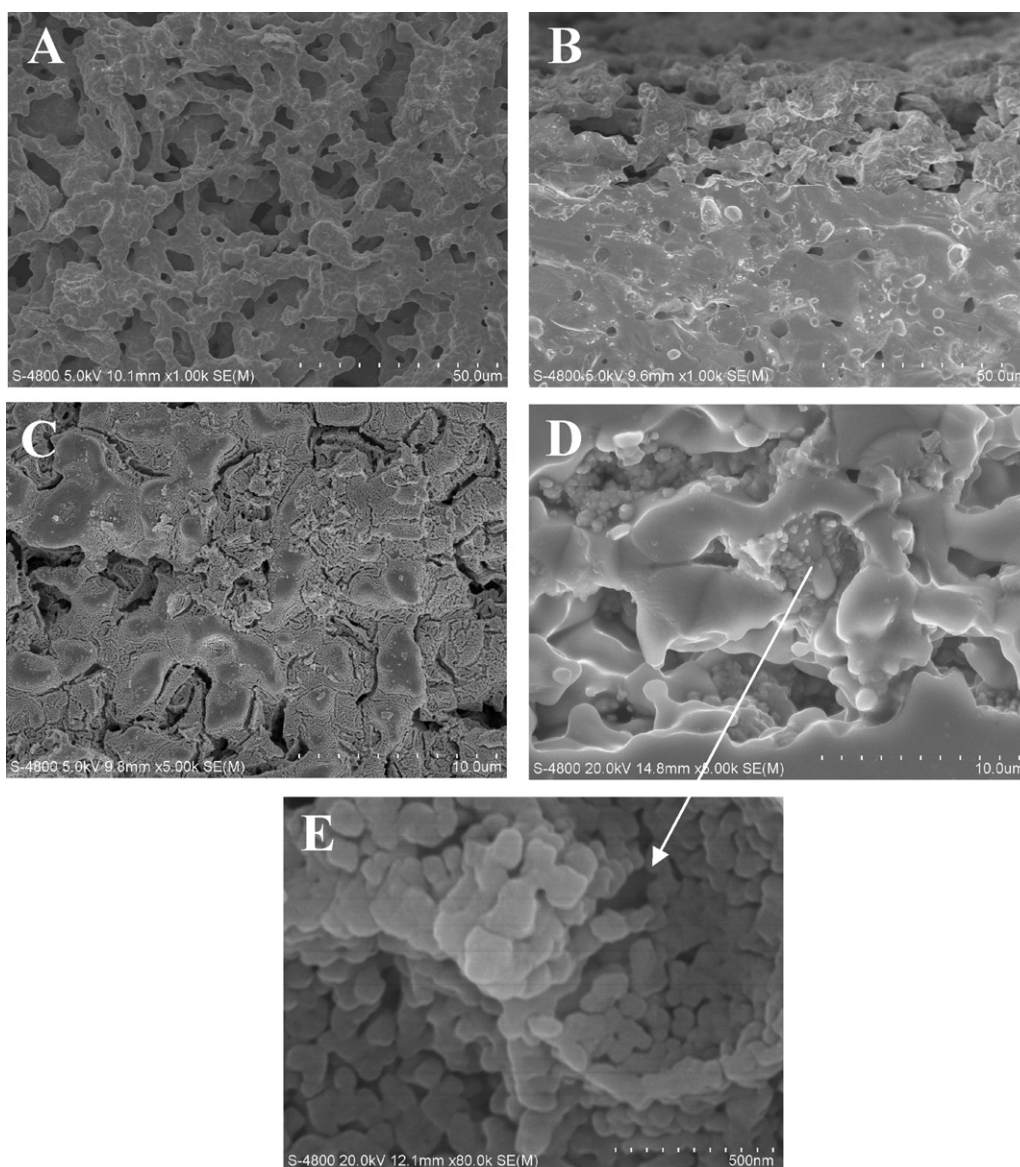


Fig. 2. XRD patterns of the porous layer without (A) and with (B) LSCM-impregnation.



**Fig. 3.** SEM images of the samples: (A) the surface without LSCM-impregnation, (B) cross-section without LSCM-impregnation, (C) the surface with LSCM-impregnation, (D) cross-section with LSCM-impregnation, (E) LSCM particles.

### 3.2. Sensing performances of the sensor

This sensor can be described by the following electrochemical cells in sample gas:  $(-)$   $O_2 + NO_2$ , LSCM/CGO/Pt,  $NO_2 + O_2 (+)$ . When the potential moves negatively from the open potential, the following electrochemical reactions will occur:

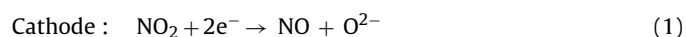


Fig. 4 shows the current–voltage ( $I$ – $V$ ) characteristics of the sensor. Potential scans from 0 to  $-300$  mV were acquired for the sensor with a scan rate of 1 mV/s under various  $NO_2$  concentrations and different operating temperatures. We can see from  $I$ – $V$  curves that the response current value increased with the negatively moving of applied potential when temperature was fixed. Moreover, with the operating temperature increasing, the response current became larger at given  $NO_2$  concentration. For example, the response currents to 300 ppm  $NO_2$  reached about 7  $\mu A$  and 120  $\mu A$  at 400 and 550  $^\circ C$ , respectively. The current for the sensor was larger than that

of the sensor using conventional sensing electrode [15,18]. At a fixed  $NO_2$  concentration, the response current depends on catalytic activities of sensing material to reaction (1) and the length of the triple phase boundary where reaction (1) takes place. In present sensor, because of nano-sized LSCM particles dispersed in porous CGO backbone as sensing material, LSCM catalytic activity is not only enhanced, but also the length of the triple phase boundary is increased due to three-dimensional contact between CGO and LSCM.

In optimizing the sensor response, choices needed to be made involving the magnitude of polarization. The polarization promotes reaction (1), but the electrode degradation can arise from coarsening of electrode microstructure at large polarization [30]. In the meanwhile, polarization can also create morphological change of the sensing electrode [31]. So, choice of  $-300$  mV for the cathodic polarization should minimize the electrode degradation and lead to a maximum current value in the polarization range.

The relationships between the response current and  $NO_2$  concentrations at the bias potential of  $-300$  mV are also shown in insets of Fig. 4. The response current was nearly linear change with  $NO_2$

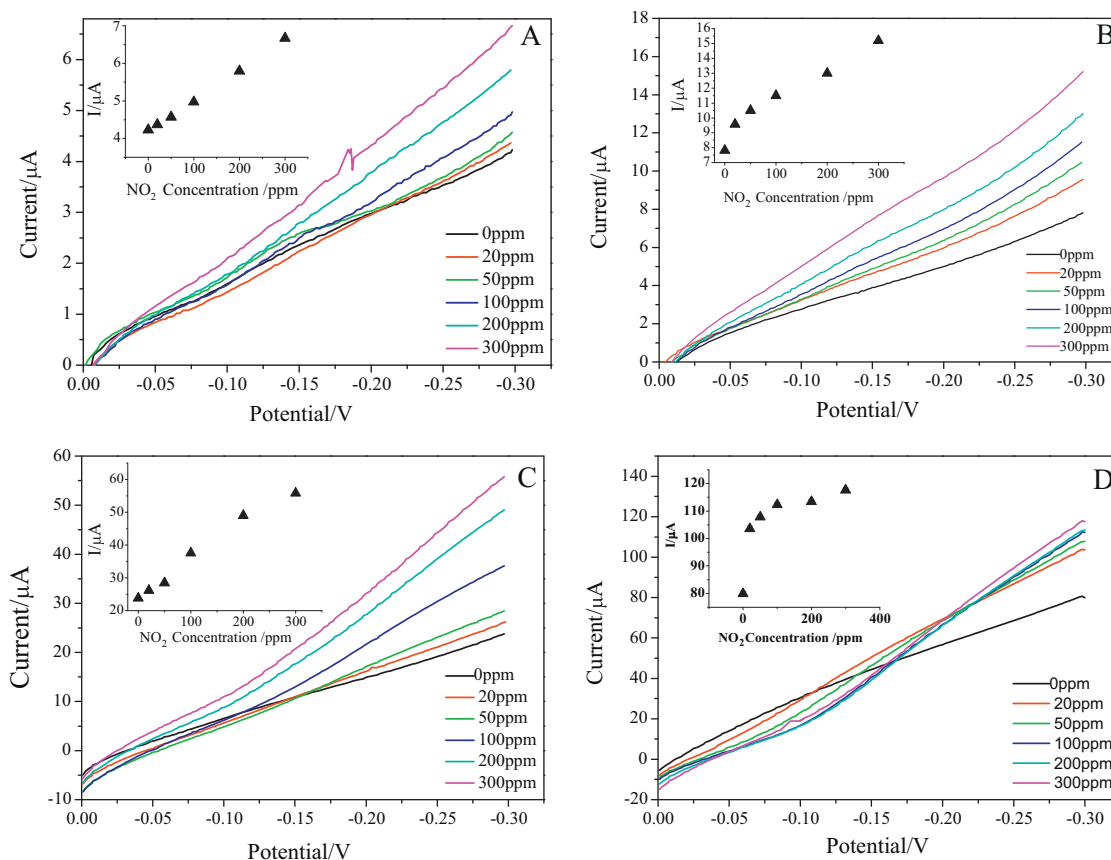


Fig. 4.  $I$ - $V$  characteristics of the sensor with various NO<sub>2</sub> concentrations at 400 °C (A), 450 °C (B), 500 °C (C) and 550 °C (D).

concentration in the range between 20 and 300 ppm at 400–500 °C. With the operating temperature increasing, the sensitivity of the sensor increase and was evaluated to be 111.36 nA ppm<sup>-1</sup> at 500 °C. However, at the operating temperature of 550 °C, there was not a linear relationship between the response current and NO<sub>2</sub> concentration. The sensitivity became lower than the one at 500 °C. The response current of the sensor stems from the electrochemical catalytic reduction of NO<sub>2</sub> at the triple phase boundary. With the temperature elevating, the chemical catalytic decomposition of NO<sub>2</sub> is increased, which results in the ratio of NO<sub>2</sub> by electrochemical catalytic reduction decreasing. Therefore, the sensitivity becomes lower.

Fig. 5 shows transient response curves of the sensor in NO<sub>2</sub> concentration from 20 to 300 ppm at 450 °C (Fig. 5A) and 500 °C (Fig. 5B), when the bias potential of -300 mV was applied. It was seen that the current values sharply increased from the base line upon switching from the base gas to the sample gas and the relatively steady current was finally attained. When the concentration of NO<sub>2</sub> was decreased to 0 ppm, the response current was reversibly returned to base line value. The sensor responded and recovered quickly as the NO<sub>2</sub> concentration was changed in every step and the base line keeps stable. The results shown in Fig. 5 were found to be highly reproducible when the concentration of NO<sub>2</sub> was switched between 0 and 300 ppm. The response time defined as time for reaching the 90% steady current is 220 s and the recovery time defined as time attaining within 10% of the initial current value is 360 s for 300 ppm NO<sub>2</sub> at 500 °C.

In addition, the response/recovery times are also influenced by the gas delivery system. Because of dead volume, it takes some time for the NO<sub>2</sub> concentrations in gas mixtures to reach a steady state in test chamber when NO<sub>2</sub> concentrations change step by step. In

support of this argument, the response current varying with time for 200 ppm NO<sub>2</sub> at two different total gas flow rates (100 and 300 cm<sup>3</sup>/min) at 500 °C was recorded and shown in Fig. 6. It can be seen that the response time was 350 s at a flow rate of 100 cm<sup>3</sup>/min. When the total flow rate was increased to 300 cm<sup>3</sup>/min, a 120 s response time was obtained. In fact, the real response/recovery time can be faster if the parameters of sensor fabrication, such as the thickness of the porous CGO layer and the loading of LSCM, are further optimized. Further characteristic optimization of this NO<sub>2</sub> sensor is under way.

It has been claimed that O<sub>2</sub> as a coexistent gas with NO<sub>2</sub> can intervene sensor response to NO<sub>2</sub> [18,23]. In order to check this point, the influence of different O<sub>2</sub> concentration on the sensor was tested and the results are shown in Fig. 7. In the presence of varying concentration of O<sub>2</sub>, a slight increase in current was noted with increasing O<sub>2</sub> concentration. The total increase in current from the change in O<sub>2</sub> between 0% and 10% was only about 1.5%.

In order to further understand the behavior of the sensor with different O<sub>2</sub> concentrations, the impedance spectra were recorded from 1 M to 0.001 Hz with (Fig. 8). The impedance spectra at high frequencies which correspond to the electrolyte behavior, overlapped each other. The result indicates that the impedance values ( $|Z|$ ) of the sensor are hardly affected by gas components, which is consistent with previous studies [10,11]. On the other hand, the impedance value at low frequencies decreased slightly with an increase in the concentration of O<sub>2</sub> in the presence of 300 ppm NO<sub>2</sub>. However, the changes of the impedance value in NO<sub>2</sub> concentration from 100 to 300 ppm were by far larger than that in O<sub>2</sub> concentration from 0 to 10% in the presence of 300 ppm NO<sub>2</sub>. So, the changes in the low-frequency behavior were much more sensitive to NO<sub>2</sub> than O<sub>2</sub>.

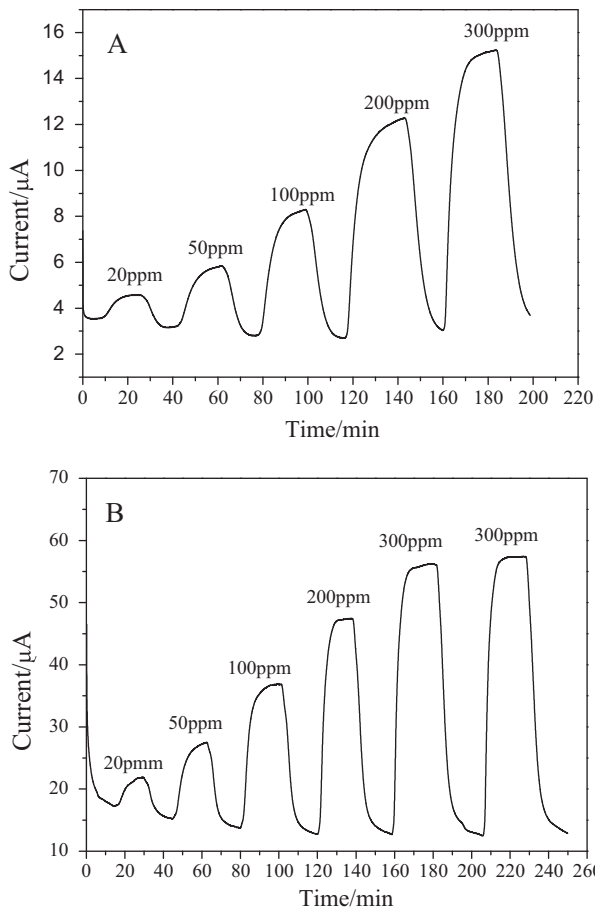


Fig. 5. Amperometric response to 20–300 ppm NO<sub>2</sub> in the presence of 5 vol.% O<sub>2</sub> at 450 °C (A) and 500 °C (B) (applied potential –300 mV, flow rate 100 cm<sup>3</sup>/min).

To test the stability of the sensor, the signal of the device was recorded over 3 h upon exposure to 300 ppm NO<sub>2</sub> gas (Fig. 9). It can be found that the current almost kept constant during the test period. When the concentration of NO<sub>2</sub> was switched from 300 to 0 ppm, the sensing current was reversibly returned to the base line which kept stable. The preliminary results reported here imply that the sensor shows good stability. Further research is being carried out for testing the long-term stability and other gas influence.

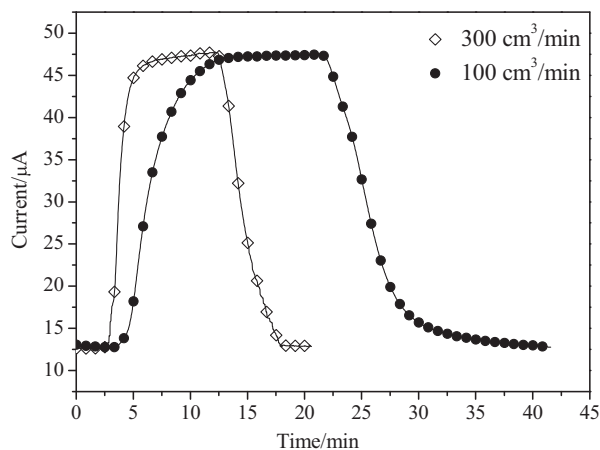


Fig. 6. Amperometric response to 200 ppm NO<sub>2</sub> in the presence of 5 vol.% O<sub>2</sub> at different total flow rates (applied potential –300 mV, 500 °C).

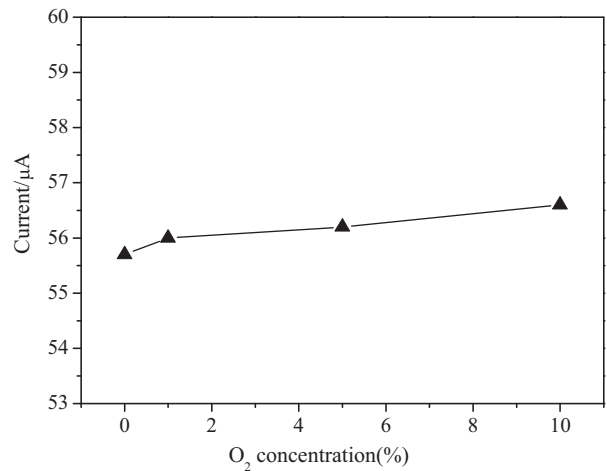


Fig. 7. Dependence of response to 300 ppm NO<sub>2</sub> on concentrations of O<sub>2</sub> (0–10 vol%) for the sensor (applied potential –300 mV, 500 °C).

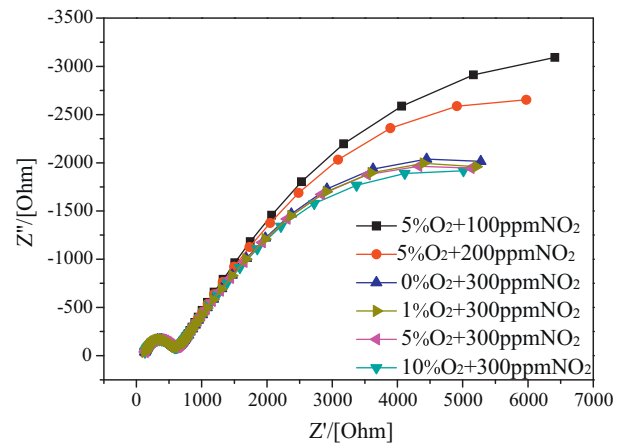


Fig. 8. Nyquist plot of samples with different O<sub>2</sub> concentration in the frequency range of 0.1 Hz to 1 MHz at 500 °C.

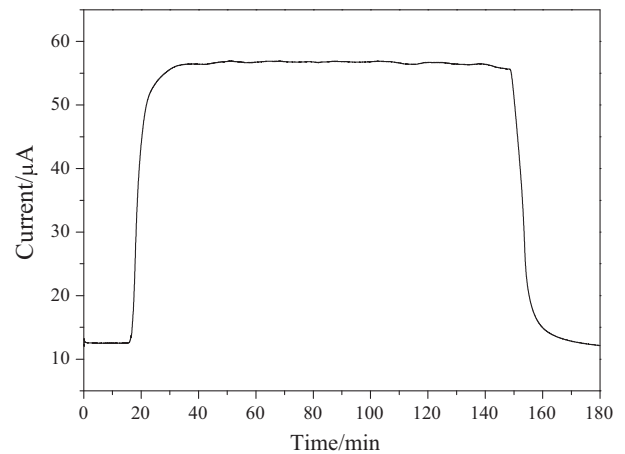


Fig. 9. Stability test for the sensor at 500 °C in the presence of 300 ppm NO<sub>2</sub> (applied potential –300 mV, flow rate 100 cm<sup>3</sup>/min).

#### 4. Conclusions

An amperometric NO<sub>2</sub> sensor based on LSCM nano-particles as sensing electrode and CGO as electrolyte was fabricated and tested. The results displayed that the ultrafine LSCM particles were

homogeneously dispersed in the porous CGO layer which greatly increase three phase boundary length ( $\text{NO}_2$  gas/LSCM/CGO). The response current was almost linear to  $\text{NO}_2$  concentration in the range between 20 and 300 ppm. With the operating temperatures increasing, the sensitivity increases at 400–500 °C. The sensor also shows high reproducibility and good stability. A negligibly increase in response current is noted with increasing  $\text{O}_2$  concentration.

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